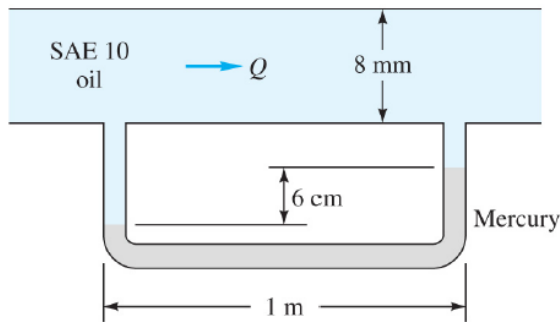


1. (P4.86 in the book) SAE 10 oil at 20°C flows between parallel plates 8 mm apart, as shown in Figure. A mercury manometer, with wall pressure taps 1 m apart, registers a 6-cm height, as shown. Estimate the flow rate of oil for this condition.



Solution: Assuming laminar flow, this geometry fits Eqs. (4.143, 144) of the text:

$$V_{\text{avg}} = \frac{2}{3} u_{\text{max}} = \left(\frac{dp}{dx} \right) \frac{h^2}{3\mu}, \quad \text{where } h = \text{plate half-width} = 4 \text{ mm}$$

For SAE 10W oil, take $\rho = 870 \text{ kg/m}^3$ and $\mu = 0.104 \text{ kg/m}\cdot\text{s}$. The manometer reads

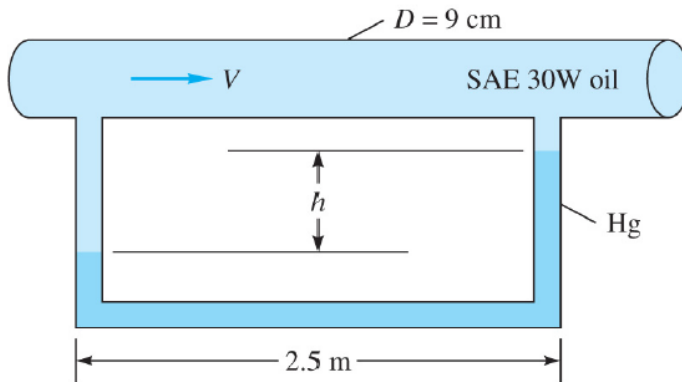
$$\Delta p = (\rho_{\text{Hg}} - \rho_{\text{oil}})g\Delta h = (13550 - 870)(9.81)(0.06) \approx 7463 \text{ Pa} \quad \text{for } \Delta x = L = 1 \text{ m}$$

$$\text{Then } V = \frac{\Delta p}{\Delta x} \frac{h^2}{3\mu} = \left(\frac{7463 \text{ Pa}}{1 \text{ m}} \right) \frac{(0.004)^2}{3(0.104)} \approx 0.383 \frac{\text{m}}{\text{s}}$$

$$\text{The flow rate per unit width is } Q = VA = (0.383)(0.008) \approx \mathbf{0.00306} \frac{\text{m}^3}{\text{s}\cdot\text{m}} \quad \text{Ans.}$$

NOTE: The Reynolds number, based upon plate half-width, is 16, *laminar*.

2. (P4.87 in the book) SAE 30 W oil at 20°C flows through the 9-cm-diameter pipe in Figure below at an average velocity of 4.3 m/s. (a) Verify that the flow is laminar, i.e., the Reynolds number $Re_d < 2300$. (b) Determine the volume flow rate in m^3/h . (c) Calculate the expected reading h of the mercury manometer, in cm.



Solution: (a) Check the Reynolds number. For SAE 30W oil, from Appendix A.3, $\rho = 891 \text{ kg/m}^3$ and $\mu = 0.29 \text{ kg/(m}\cdot\text{s)}$. Then

$$Re_d = \rho V d / \mu = (891 \text{ kg/m}^3)(4.3 \text{ m/s})(0.09 \text{ m}) / [0.29 \text{ kg/(m}\cdot\text{s)}] = 1190 < 2000 \text{ Laminar} \quad \text{Ans. (a)}$$

(b) With average velocity known, the volume flow follows easily:

$$Q = AV = [(\pi/4)(0.09 \text{ m})^2](4.3 \text{ m/s})(3600 \text{ s/h}) = \mathbf{98.5 \text{ m}^3/\text{h}} \quad \text{Ans. (b)}$$

(c) The manometer measures the pressure drop over a 2.5 m length of pipe. From Eq. (4.147),

$$V = 4.3 \frac{\text{m}}{\text{s}} = \frac{\Delta p R^2}{L 8\mu} = \frac{\Delta p}{2.5 \text{ m}} \frac{(0.045 \text{ m})^2}{8(0.29 \text{ kg/m}\cdot\text{s})}, \quad \text{solve for } \Delta p = 12320 \text{ Pa}$$

$$\Delta p_{\text{mano}} = 12320 = (\rho_{\text{merc}} - \rho_{\text{oil}})gh = (13550 - 891)(9.81)h, \quad \text{Solve } \mathbf{h = 0.099 \text{ m}} \quad \text{Ans. (c)}$$

3. (P4.90 in the book) It is desired to pump ethanol at 20°C through 25 m of straight smooth tubing under laminar-flow conditions, $Re_d = \frac{\rho V d}{\mu} < 2300$. The available pressure drop is 10 kPa. (a) What is the maximum possible mass flow, in kg/h. (b) What is the appropriate diameter?

Solution: For ethanol at 20°C, $\rho = 789 \text{ kg/m}^3$ and $\mu = 0.0012 \text{ kg/m}\cdot\text{s}$. From Eq. (4.138),

$$Q_{\text{laminar}} = \frac{\pi R^4}{8\mu} \frac{\Delta p}{L} = \frac{\pi d^4}{128\mu} \frac{\Delta p}{L}$$

Clearly, flow increases with diameter, so maximum mass flow requires the maximum diameter consistent with the maximum Reynolds number. The Reynolds number may be written out:

$$Re_d = \frac{\rho V d}{\mu} = \frac{4\rho Q}{\pi d \mu} = \left(\frac{4\rho}{\pi d \mu}\right) \left(\frac{\pi d^4}{128\mu} \frac{\Delta p}{L}\right) = \frac{\rho d^3 \Delta p}{32\mu^2 L} < 2300$$

$$\text{Or: } d^3 = \frac{2300(32)\mu^2 L}{\rho \Delta p} = \frac{2300(32)(0.0012)^2(25)}{(789)(10,000)} = 3.36E-7 \text{ m}^3$$

$$\text{Solve for } d_{\text{max}} = 0.00695 \text{ m} \approx 7 \text{ mm} \quad \text{Ans. (b)}$$

The maximum mass flow is

$$\dot{m}_{\text{max}} = \rho Q_{\text{max}} = (789 \frac{\text{kg}}{\text{m}^3}) \left[\frac{\pi(0.00695 \text{ m})^4}{128(0.0012 \text{ kg/m}\cdot\text{s})} \right] \left(\frac{10,000 \text{ Pa}}{25 \text{ m}} \right) = 0.0151 \frac{\text{kg}}{\text{s}} = 54 \frac{\text{kg}}{\text{h}} \quad \text{Ans. (a)}$$

Light liquids like ethanol stay laminar only for tiny diameters. To work the same problem with, say, SAE 30W oil, $\mu = 0.29 \text{ kg/m}\cdot\text{s}$, would result in $d_{\text{max}} = 26 \text{ cm}$, or 37 times larger. The maximum oil mass flow would be nearly nine thousand times larger.

4. **(P4.93 in the book)** A number of straight 25-cm-long microtubes of diameter d are bundled together into a “honeycomb” whose total cross-sectional area is 0.0006 m^2 . The pressure drop from the entrance to exit is 1.5 kPa. It is desired that the total volume flow rate be $1 \text{ m}^3/\text{h}$ of water at 20°C . (a) What is the appropriate microtube diameter? (b) How many microtubes are in the bundle? (c) What is the Reynolds number of each microtube?

Solution: For water at 20°C , $\rho = 998 \text{ kg/m}^3$ and $\mu = 0.001 \text{ kg/m}\cdot\text{s}$. Each microtube of diameter D sees the same pressure drop. If there are N tubes,

$$Q = \frac{1}{3600} \frac{\text{m}^3}{\text{s}} = N Q_{\text{tube}} = N \frac{\pi D^4 \Delta p}{128 \mu L} = N \frac{\pi D^4 (1500 \text{ Pa})}{128 (0.001 \text{ kg/m}\cdot\text{s})(0.25 \text{ m})} = 1.47E5 N D^4$$

$$\text{At the same time, } N = A_{\text{bundle}}/A_{\text{tube}} = \frac{0.0006 \text{ m}^2}{(\pi/4)D^2}$$

Combine to find $D^2 = 2.47E-6 \text{ m}^2$ or $D = 0.00157 \text{ m}$ and $N = 310$ Ans.(a, b)

With D known, compute $V = Q/A_{\text{bundle}} = Q_{\text{tube}}/A_{\text{tube}} = 0.462 \text{ m/s}$ and

$$\text{Re}D = \rho V D / \mu = (998)(0.462)(0.00157)/(0.001) = 724 \text{ (laminar)} \quad \text{Ans. (c)}$$

5. (P4.94 in the book) A long solid cylinder rotates steadily in a very viscous fluid, as in Fig. P4.94. Assuming laminar flow, solve the Navier-Stokes equation in polar coordinates to determine the resulting velocity distribution. The fluid is at rest far from the cylinder. [Hint: the cylinder does not induce any radial motion.]

Solution: We already have the useful hint that $v_r = 0$. Continuity then tells us that

$(1/r)\partial v_\theta/\partial\theta = 0$, hence v_θ does not vary with θ . Navier-Stokes then yields the flow. From Eq. D.6, the tangential momentum relation, with $\partial p/\partial\theta = 0$ and $v_\theta = f(r)$, we obtain Eq. (4.139):

$$\frac{1}{r} \frac{d}{dr} \left(r \frac{dv_\theta}{dr} \right) = \frac{v_\theta}{r^2}, \quad \text{Solution: } v_\theta = C_1 r + \frac{C_2}{r}$$

As $r \rightarrow \infty$, $v_\theta \rightarrow 0$, hence $C_1 = 0$

$$\text{At } r = R, \quad v_\theta = \Omega R = \frac{C_2}{R}; \quad C_2 = \Omega R^2; \quad \text{Finally, } v_\theta = \frac{\Omega R^2}{r} \quad \text{Ans.}$$

Rotating a cylinder in a large expanse of fluid sets up (eventually) a potential vortex flow.