4th AIAA CFD Drag Prediction Workshop



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Outline



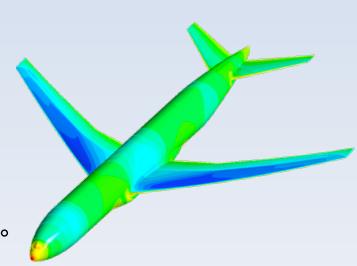
- Test cases
- Grid
- Setup
- Results
- Computational info
- Summary



Test cases



- Case 1.1: Grid convergence study
 - Mach = 0.85, $c_L = 0.500 (\pm 0.001)$
 - Chord Reynolds Number 5x10⁶
 - Coarse, medium, fine, extra-fine
- Case 1.2: Downwash study
 - Mach = 0.85, $c_L = 0.500 (\pm 0.001)$
 - Chord Reynolds Number 5x10⁶
 - AoA 0.0°, 1.0°, 1.5°, 2.0°, 2.5°, 3.0°, 4.0°
 - i_H = -2°, 0°, +2° and tail off
- Case 3: Reynolds number study
 - Mach 0.85, $c_L = 0.500 (\pm 0.001)$
 - Chord Reynolds Number 20x10⁶
 - Medium

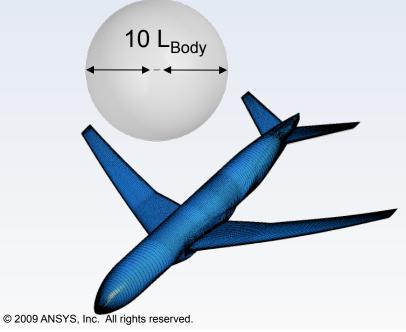




Grid



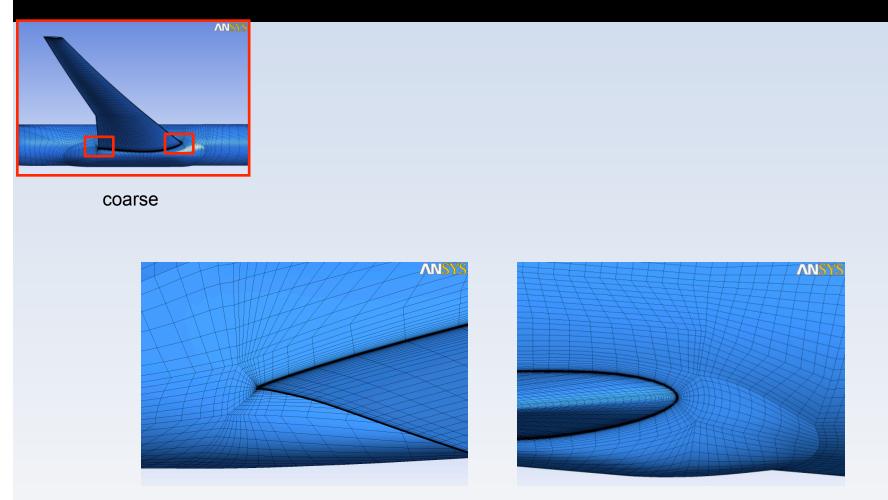
- ANSYS ICEM CFD
- Multiblock structured mesher
- Top-down meshing
- Hexahedral mesh



	Coarse	Medium	Fine	Extra-Fine	
Nodes	3,592,043	10,951,602	36,159,816	104,991,542	
Elements	3,516,705	10,793,559	35,808,564	104,273,186	
Min. angle	14°	14°	12°	11°	
Max. skewness	0.96	0.96	0.96	0.96	
Max. volume change	11	10	12	14	
Max. aspect ratio	62,000	61,000	65,000	65,000	
# cells across TE	7	12	18 24		

Grid - Coarse

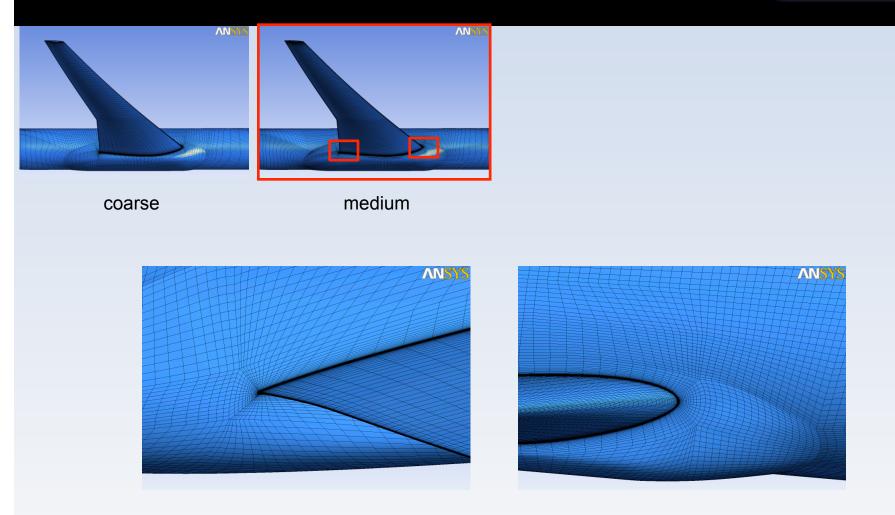




3,516,705 hexahedral cells 150,044 boundary faces

Grid - Medium

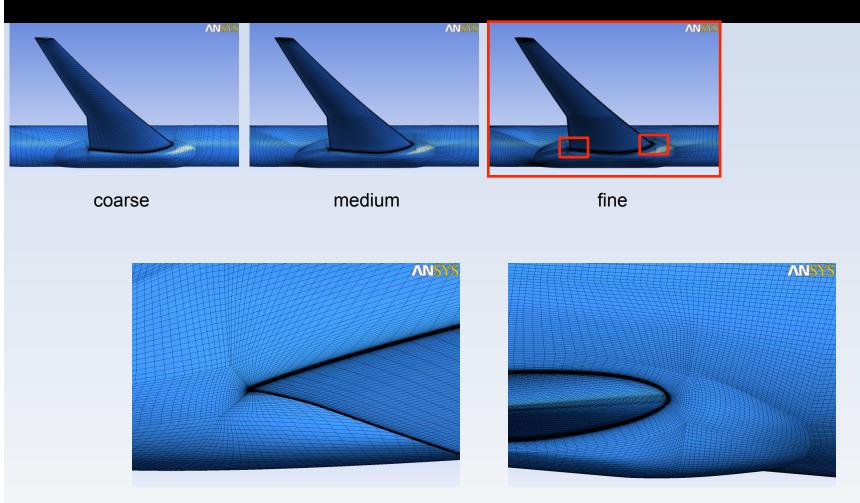




10,793,559 hexahedral cells 315,162 boundary faces

Grid - Fine

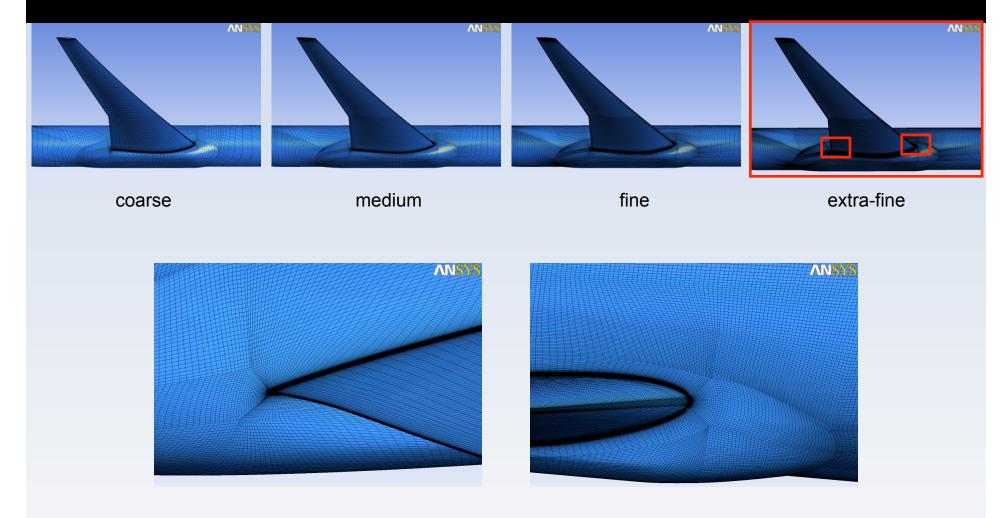




35,808,564 hexahedral cells 701,124 boundary faces

Grid – Extra-Fine



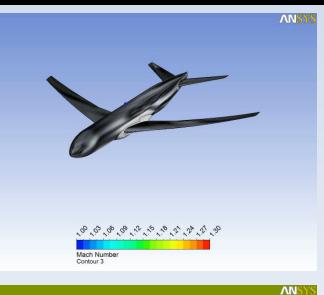


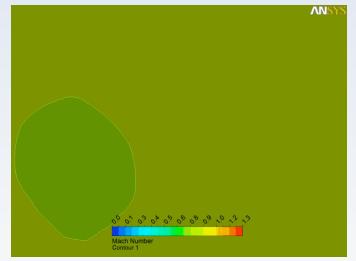
104,273,186 hexahedral cells 1,434,740 boundary faces

Setup - Solver



- ANSYS FLUENT 12
- Steady state
- Compressible (ideal gas)
- Density-based implicit coupled solver
- Spatial discretization: 2nd order
- Least-square cell-based gradient
- Flux Type: Roe-FDS
- Algebraic multigrid method
- Scalable parallelization
- Double precision

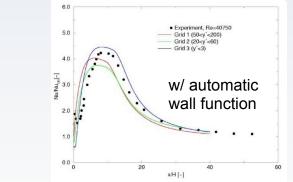


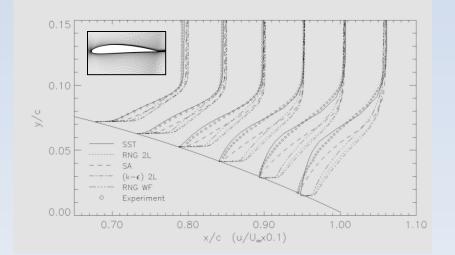


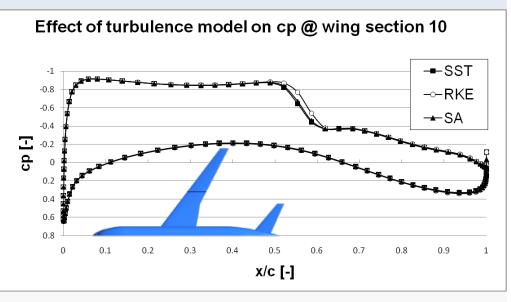
Setup - Model error



- SST model (Menter, 1994)
 - Blending of k- ϵ and k- ω model
 - Improved eddy viscosity formula
- Proper model for separated flows
- Automatic wall function
 - Less sensitive to y⁺





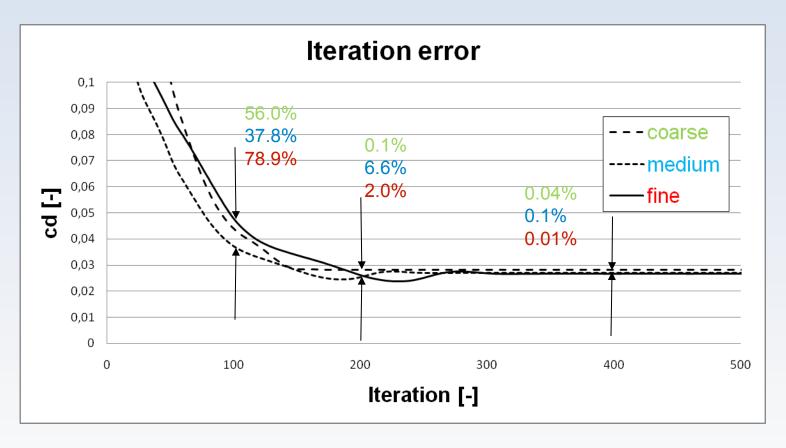


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Results – Iteration error



- 400 iterations for convergence (relative error $\leq 0.1\%$)
- Converged within 1 drag count



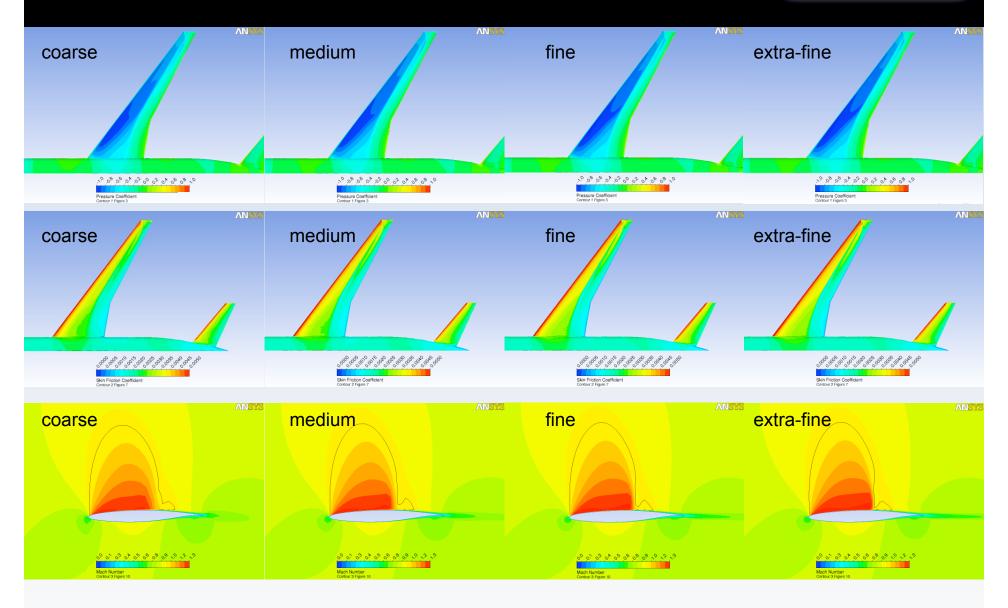
Results – Discretization error



Effect of discretization on cp @ wing section 14 -0.7 Increasing discretization error -0.4 -0 5 with increasing distance to -coarse **-**0.4 **d** -0.3 ---medium fuselage + fine extra-fine -0.2 Fine and extra-fine results -0.1 0 almost congruent 0.5 0.55 0.4 0.45 0.6 x/c [-] Effect of discretization on cp @ wing section 4 Effect of discretization on cp @ wing section 10 -0.6 ---coarse --coarse -1 -0.5 -∽–medium -0.8 -fine + fine -0.4 extra-fine -0.6 cp [-] extra-fine cp [-] -0.3 -0.4 -0.2 -0.2 0 -0.1 0.2 0 0.55 0.6 0.5 0.65 0.7 0.6 0.62 0.64 0.66 0.68 07 0.72 0 74 0.76 0.78 0.8 x/c [-] x/c [-] 12 © 2009 ANSYS, Inc. All rights reserved. ANSYS, Inc. Proprietary

Results – Discretization error

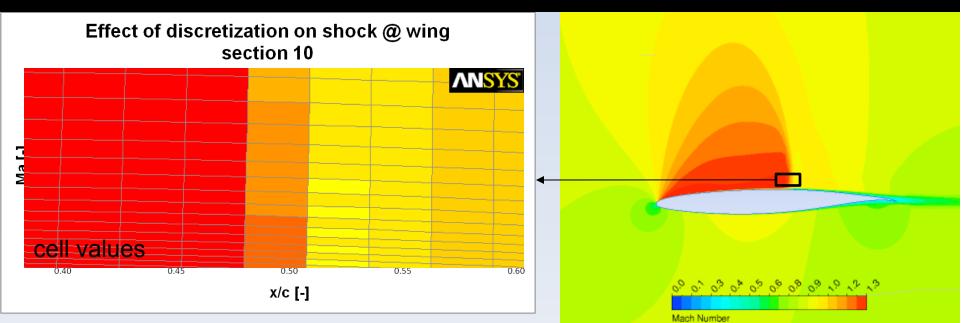




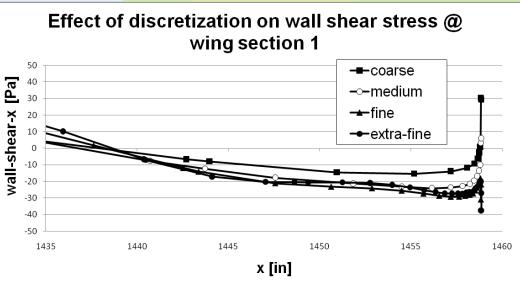
ANSYS[®] **Results – Discretization error** AN ANS medium extra-fine fine coarse ANSY ANSY **ANSY** AN medium fine extra-fine coarse Wall Shear X Wall Shear X **ANS ANS** ANS ANS medium fine extra-fine coarse iso-surface of $v_x = -10$ m/s

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Results – Discretization error



 Finer mesh leads to increased wall-shear-xstresses and enlarged separation bubble



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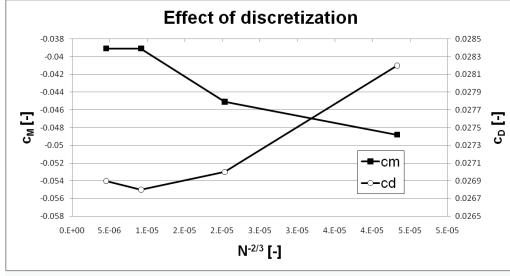
Results – Discretization error



• $c_L = 0.500 (\pm 0.001)$

• Re = 5x10⁶

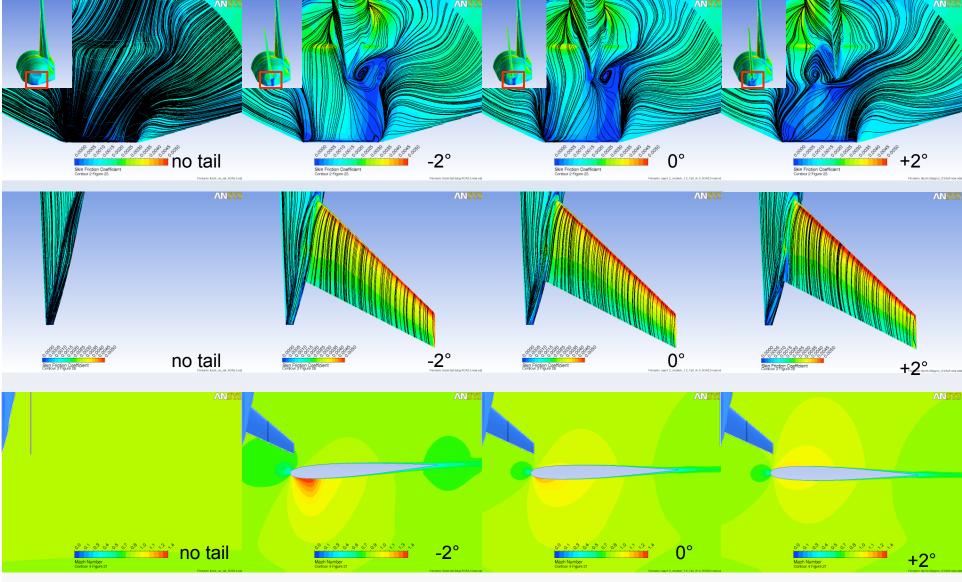
	Coarse	Medium	Fine	Extra-Fine	
Nodes	3,592,043	10,951,602	36,159,816	104,991,542	
Elements	3,516,705	10,793,559	35,808,564	104,273,186	
AoA [°]	2.209	2.260	2.308	2.339	
с _D	0.0282	0.0270	0.0268	0.0269	
С _М	-0.0488	-0.0451	-0.0391	-0.0391	
y⁺ _{avg}	0.358	0.242	0.163	0.110	



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Results – Downwash study

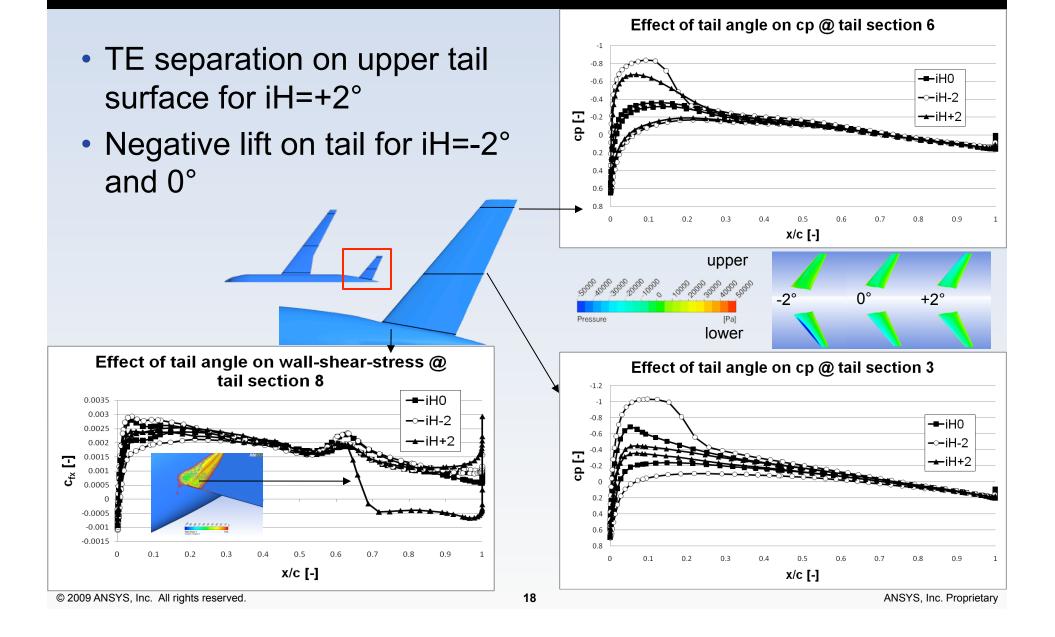




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Results – Downwash study





Results – Downwash study

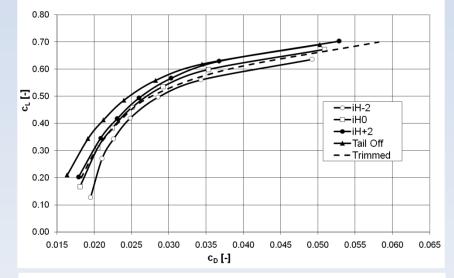


0.80 0.70 0.60 ±0.50 പ -□--iH0 **→**iH+2 0.40 ----- Tail Off 0.30 – Trimmed 0.20 0.10 0.00 0.0 0.5 1.0 1.5 2.0 2.5 3.0 3.5 4.0 4.5 5.0 AoA [°]

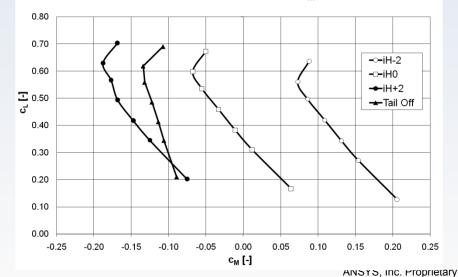
Effect of Stabilizer Angle on c

Effect of trimming on i_H and AoA 1.00 c_L≠ 0.2 0.80 0.60 $c_1 = 0.3$ 0.40 0.20 ed [°] 0.00 c_l = 0.4 -0.20 н Н -c_L= 0.7 -0.40 c_l = 0.5 -0.60 -0.80 -1.00 ¢, = 0.6 -1.20 0.00 0.50 1.00 1.50 2.00 2.50 3.00 3.50 4.00 4.50 5.00 AoA_{trimmed} [°]

Effect of Stabilizer Angle on c_D





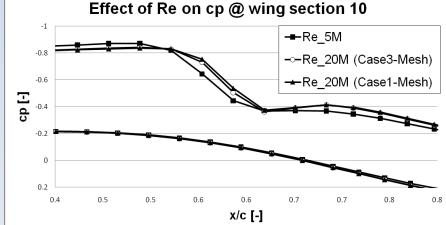


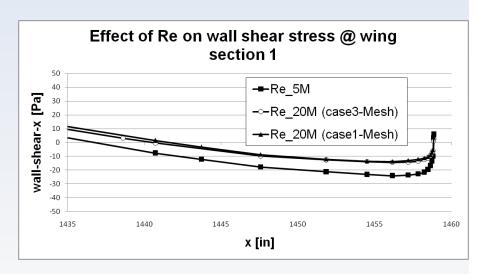
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Results – Reynolds Number study (NSYS)

- Increased Reynolds number shifts shock towards TE
- Delayed TE separation and decreased wall shear stresses

	Re=5x10 ⁶	Re=20x10 ⁶ (Case1- Mesh)	Re=20x10 ⁶ (Case3- Mesh)
Nodes	10,951,602	10,951,602	11,284,694
Elements	10,793,559	10,793,559	11,123,320
AoA [°]	2.2597	2.0210	2.0505
C _D	0.0270	0.0233	0.0235
C _M	-0.0451	-0.0507	-0.0507
y⁺ _{avg}	0.242	0.890	0.252





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Computational Info



	Coarse	Medium	Medium (tail off)	Medium Re=20M	Fine	Extra-Fine
Elements	3,516,705	10,793,559	8,565,287	11,123,320	35,808,564	104,273,186
Wall clock time (500 it) [h]	3.4	3.5	2.5	2.9	2.0	3.8
CPU time (500 it) [h]	26.3	119.8	77.9	91.6	386.1	1131.1
RAM usage [GB]	16.3	47.8	43.8	51.6	199.2	549.7
CPU info	8 x AMD Opteron 2.3 GHz	32 x AMD Opteron 2.3 GHz		192 x AMD Opteron 2.3 GHz	244 x AMD Opteron 2.3 GHz	
OS	SLE 10					

Summary



- Consistent and robust solver convergence
- Expected grid refinement trends are observed
 - At wing tip, grids are still not sufficiently refined
- In spite of new fairing, there are small separation bubbles on upper wing surface close to fuselage
- Blind study and unavailability of experimental data doesn't allow to comment on absolute accuracy
- Quick results even for extra-fine grid, but high RAM usage due to density-based implicit solver in double precision

Acknowledgement



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