

Electric Field Characteristics under Three-phase Voltage in Three-phase Gas Insulated Switchgear

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Abstract: This paper deals with electric field characteristics under three-phase voltage in three-phase gas insulated switchgear (GIS). Three-phase equipment differs from single-phase equipment in two aspects: configuration and applied voltage. In this paper the effects of these differences on electric field in three-phase GIS are reported. There are periodic changes in the electric field magnitude and direction produced by three-phase voltage at any point. While the voltage phase varies, the electric field vector changes and rotates continuously. The rotating characteristics of the electric field vector in three-phase power apparatus depended on the position inside the insulation of the tank. The electric field vector locus is circular, elliptic, or linear. The elliptical nature of rotating electric field is expressed as electric field ratio. The mathematic description of the rotating electric field is given considering the maximum and the minimum electric field and the position inside the insulation. There is no zero electric field under three-phase voltage. The areal velocity of the electric field vector locus is constant. The electric field vector moves slowly in a high electric field area, but moves quickly in a low electric field area.

Keywords: three-phase, rotating electric field, vector locus

1. Introduction

Application of three-phase equipment (three-phase in one tank) such as three-phase gas insulated switchgear (GIS) and three-phase gas insulated bus (GIB), has been increasing due to its compactness and low cost [1-9]. A three-phase in one-tank design has also been developed for 550 kV GIS [7]. Therefore, the knowledge on the electric field inside three-phase electric power apparatuses under three-phase voltage is very important. The knowledge on three-phase electric field is useful for electric equipment and insulation design and analyzing electric phenomena inside the insulation of equipment such as electric stress and internal discharges. Three-phase equipment differs from single-phase equipment in two aspects: configuration and applied voltage as shown in Figure 1. It can be expected that the electric field characteristic will be different from that in single-phase equipment. In this paper the effects of these differences on electric field inside three-phase GIS are studied.

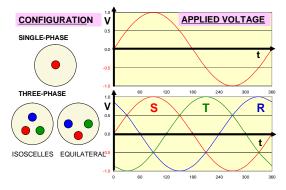


Figure 1. The difference between single-phase and three-phase equipment

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2. Model of Three-Phase GIS

A simplified model of three phase GIS was used in this research. It was composed of a tank model 150 mm in diameter, 300 mm in length, 2 mm in thickness, and three-phase conductors 25 mm in diameter.

The electrode system was arranged to simulate three-phase electric field in three-phase equipment. The conductors were arranged in an isosceles triangle construction. The layout and dimensions of the model are shown in Figure 2.

3. Electric Field Calculation

The calculation method of electric field inside three-phase equipment has been developed since more than thirty years ago [11-17]. The newest simulation method and the result in three-phase electric field calculation are described in [17].

In this research the electric fields inside the insulation of the construction were determined from a boundary element method simulation: along a circle among the phases and the tank, along vertical line starting from the bottom of the tank, along line connecting the centers of conductor phases, and around the conductor. The electric field calculation is two dimensional.

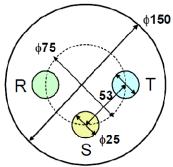


Figure 2. Layout of simplified model of three-phase gas insulated switchgear

4. Electric Field Analysis and Discussion

A. Distribution of Three-phase Electric Field

Figure 3 shows the change of electric field distribution with phase of applied voltage. Here, θ s is the phase angle of S phase of applied voltage. The blue color in the figure reveals that the electric field intensity is the lowest, while the red color reveals that the electric field intensity is the highest. The electric field distribution pattern varies with phase of applied voltage. Every a half cycle the pattern of electric field stress is repetitive.

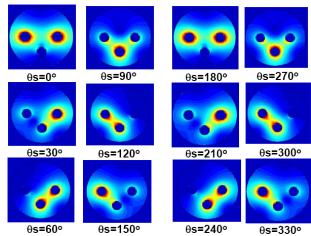


Figure 3. Change of electric field distribution with phase of applied voltage

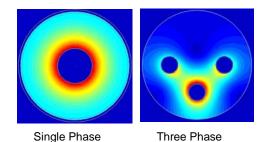


Figure 4. Electric field distributions inside single-phase equipment and three-phase GIS

Figure 4 shows the difference in electric field distribution between single-phase and threephase equipment. The electric field distribution pattern in single-phase equipment is independent of phase of applied voltage, while one in three-phase equipment changes with the change of applied voltage.

B. Periodic Changes of Electric Field Vector under Three-phase Voltage

Figure 5 shows the change in the pattern of the electric field vector at 5 mm below the center of the tank during one cycle of applied voltage. It seems that there are periodic changes in electric field magnitude and direction produced by three-phase voltage at any point. While the voltage phase varies from 0 to 2π , the electric field vector changes and rotates continuously. Note, that there is no zero electric field in three-phase construction. When the voltage of one of phases equals to zero, the voltage in the other phases is not zero.

These results differ significantly with the electric field vector characteristics inside single phase GIS under single phase voltage. Figure 6 shows the change in the pattern of the electric field vector anywhere inside single-phase GIS during one cycle of applied voltage.

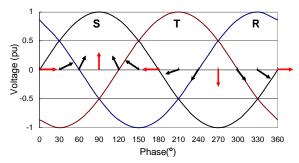


Figure 5. Pattern of the electric field vector at 5 mm below the center of the tank of three-phase GIS during one cycle of applied voltage

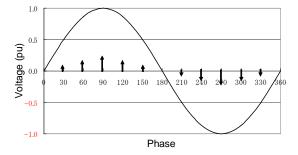


Figure 6. Pattern of the electric field vector during one cycle of applied voltage in single-phase GIS

The magnitude of electric field vector changes with the applied voltage, but the electric field vector direction is unchanged during half cycle. During the other half cycle, the directions of the electric field vector become the opposite. Note, that there are zero electric fields in single-phase construction. When the voltage is zero, the electric field is zero.

C. Rotating Characteristics of Three-phase Electric Field Vector

Figure 7 shows the change of the electric field vector at 5 mm below the center of the tank of three-phase GIS during one cycle of applied voltage in three-phase equipment. The locus is drawn based on the pattern of electric field vector in Figure 4.

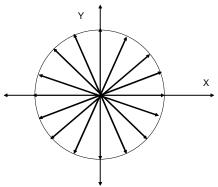


Figure 7. Locus of the electric field vector at 5 mm below the centre of the tank of three-phase GIS during one cycle of applied voltage

It appears that the electric field vector direction rotates and changes continuously. The electric field locus is circular during one cycle of applied voltage. Note, that there is no zero electric field in three-phase construction.

These results differ significantly with the electric field vector locus inside single phase GIS under single phase voltage. Figure 8 shows the electric field vector locus anywhere inside single-phase GIS during one cycle of applied voltage.

The magnitude of electric field vector changes with the applied voltage, but the electric field vector direction is unchanged during half cycle. During the other half cycle, the direction of the electric field vector becomes the opposite. There are zero electric fields in single-phase construction. When the voltage is zero, the electric field is zero.

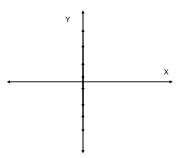


Figure 8. Locus of the electric field vector during one cycle of applied voltage in single-phase GIS

D. Pattern and Locus of Rotating Electric Field Vector

Figure 9 shows the locus of the electric field vector at different points. Here, while the vector locus is elliptic, its shape varies locally. On the electrode surface the locus is linear because the electric field lines are vertical to the conductor surface.

At some regions, for example at point A, the locus is elliptic. Meanwhile, at point B, which is 5 mm below the centre of the tank, the locus is truly circular. It is also found that the electric field vector locus between the phases and the tank is almost linear, resembling that in a single-phase configuration; while that between phases has variations: linear, elliptic, and circular.

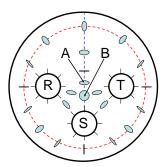


Figure 9. Electric field vector loci in isosceles triangle arrangement of three-phase construction without particle

E. The Mathematics Description of Rotating Electric Field Vector

The rotating electric field at a certain position (x,y) can be described by four parameters: the maximum Emax (x,y) and minimum Emin (x,y) field strength, the phase angle of applied voltage θ max (x,y) at maximum field Emax (x,y), and field direction ϕ max (x,y) at maximum field [11]. These parameters are illustrated in Figure 10.

 δ_{V} in the figure is defined as the angle that designates the intersection width of the electric field vector locus and critical electric field circle Ecr.

The elliptical nature of rotating electric field is expressed as electric field ratio, η . It is defined as the ratio between the magnitudes of the elliptical field along the main axes,

$$\eta = \text{Emin} / \text{Emax} (0 < \eta < 1)$$

where:

Emin: minimum electric field intensity at a certain point during a cycle of applied voltage Emax: maximum electric field intensity at a certain point during a cycle of applied voltage

When the electric field ratio $\eta = 0$, the electric field vector locus is linear. When the electric field ratio $0 < \eta < 1$, the electric field vector locus is elliptic. When the electric field ratio $\eta = 1$, the electric field vector locus is circular.

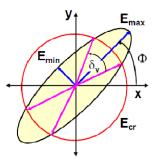


Figure 10. Rotating electric field parameters

F. Elliptical Nature of The Electric Field Vector Locus

The electric field vector locus at different points, those are at the distances 0 mm (A), 5 mm (B), 10 mm (C), 15 mm (D), 20mm (E), and 25 mm (F) away from S conductor in the absence of particle are shown in Figure 11. The points are laid between S conductor and the center of

three-phase GIS. The electric field ratio changes from $\eta = 0$ at S conductor surface (point A) to $\eta = 0.2$ at point B, $\eta = 0.4$ at point C, $\eta = 0.7$ at point D, $\eta = 1$ at point E.

Here, while the vector locus is elliptic, its shape varies locally. On the electrode surface (at Point A) the locus is linear because the electric field lines are vertical to the conductor surface. At some regions, for example at point B, C, D, the locus is elliptic. Meanwhile, at point E, which is 5 mm below the center of the tank, the locus is truly circular.

If a point approaches the center of the cross section of the tank, the maximum electric field reduces; while the minimum electric field increases as shown in Figure 12. The minimum and maximum electric fields are same at point E (20 mm from S conductor). The electric field vector locus changes from linear to circular when the points keep away from S conductor (point A) to the point 5 mm below the center of the three-phase construction (point E). The electric field ratio (η) changes from 0 until 1 from point A until E.

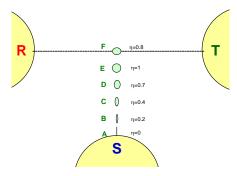


Figure 11. The electric field vector locus at the distances 0 mm (A), 5 mm (B), 10 mm (C), 15 mm (D), 20mm (E), and 25 mm (F) away from S conductor

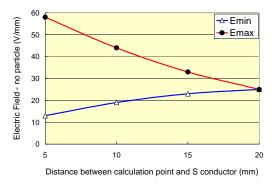


Figure 12. Minimum and maximum electric field from point B (5mm from S conductor) until point E(20mm from S conductor) without particle

G. Rotating Electric Field Characteristics

Figure 13 illustrates the absolute electric field for three different positions during a cycle of the applied voltage V_a . E_{max} at each position is the same, while the electric field ratio η is different, designated by η_1 , η_2 , and η_3 , where $\eta_1 > \eta_2 > \eta_3$.

It is clear that at a certain position (x,y) inside the three-phase construction, the field is rotating with varying magnitudes, i.e, sinusoidal in two perpendicular directions without necessarily coinciding at zero crossings. For the same maximum electric field, there may be various values of the electric field ratio η at different positions.

The other important characteristic of three-phase electric field is the difference in the angular velocity of the applied voltage and the angular velocity of the electric field vector. The

angular velocity of the applied voltage Va is constant, while the angular velocity of the electric field always changes. The areal velocity of the electric field vector locus is constant. The electric field vector moves slowly ina high electric field area, but moves quickly in a low electric field area.

 $vavr = v = \omega \min Emax = \omega \max Emin$

The maximum angular velocity ω max of electric field vector locus is estimated as change in the direction of the electric field vector with time at minimum electric field, i.e.

 $\omega_{\text{max}} = d\varphi / dt$ at $E = E_{\text{min}}$

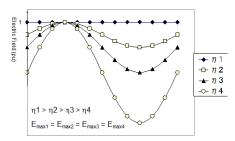


Figure 13. The absolute electric field for three different positions during a cycle of the applied voltage V_a

5. Conclusions

Three-phase equipment differs from single-phase equipment in two aspects: configuration and applied voltage. In this paper effects of these differences on the electric field in three-phase gas insulated system (GIS) are reported. The electric field in a three-phase construction of a simplified GIS model was analyzed. The following conclusions were drawn:

- 1. The electric field distribution pattern varies with phase of applied voltage.
- 2. Every a half cycle the pattern of electric field stress is repetitive.
- 3. There are periodic changes in the electric field magnitude and direction produced by threephase voltage at any point.
- 4. While the voltage phase varies from 0 to 2π , the electric field vector changes and rotates continuously.
- 5. There is no zero electric field in three-phase construction.
- 6. The results are compared with the electric field characteristics under single-phase voltage in single-phase electric power apparatuses.
- 7. Electric field vector locus in the region between conductor and the enclosure is almost linear, resembling a single-phase construction; while ones between conductors have variations: linear, elliptic, circular.
- 8. The elliptical nature of rotating electric field is expressed as electric field ratio. The mathematic description of the rotating electric field is given considering the maximum and the minimum electric field and the position inside the insulation.
- 9. The areal velocity of the electric field vector locus is constant. The electric field vector moves slowly in a high electric field area, but moves quickly in a low electric field area.

The results are compared with the electric field characteristics under single-phase voltage in single-phase electric power apparatuses. There is a distinct difference between electrical field characteristics of single-phase and three-phase configurations.

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References

- [1] S. Okabe, S. Kaneko, M. Yoshimura, H. Muto, C. Nishida, M. Kamei, "Propagation Characteristics of Electromagnetic Waves in Three-Phase-Type Tank from Viewpoint of Partial Discharge Diagnosis on Gas Insulated Switchgear," *IEEE Transactions on Dielectrics and Electrical Insulation*", Vol. 16, No. 1, pp. 199-205, 2009.
- [2] Umar Khayam, Nobuko Otaka, Takakazu Matsuyama, Yoshiki Takehara, Shinya Ohtsuka, Masayuki Hikita, "Examination of Single Phase PDM Device for PD Diagnosis on Three-phase GIS", *International Journal on Electrical Engineering and Informatics*, Vol. 2 No. 3, pp 244-255, 2010.
- [3] S. Yanabu, H. Okubo, S. Matsumoto: "Metallic Particle Motion in Three-phase SF6 Gas Insulated Bus", *IEEE Transactions on Power Delivery Vol. PWRD-2, No. 1, pp. 1-6, January 1987.*
- [4] Umar Khayam, S. Ohtsuka, S. Matsumoto, M. Hikita, "Partial Discharge and Cross Interference Phenomena in a Three-phase Construction", *International Journal on Electrical Engineering and Informatics*, Vol. 1, No.1, pp. 78-91, 2009.
- [5] E. Harkink, F.H. Kreuger, P.H.F. Morshuis: "Partial Discharges in Three-core Belted Power Cables", *IEEE Transactions on Electrical Insulation*, Vol. 24, No. 4, pp. 591-598, 1989.
- [6] Umar Khayam, T. Ishitobi, S. Ohtsuka, S. Matsumoto, M. Hikita, "Effect of Elliptical Nature of Rotating Electric Field on Partial Discharge Pattern in a Three-phase Construction", *IEEJ Transaction on Fundamentals and Materials*, Vol. 127, No.9, pp. 524-530, 2007.
- [7] S. Yanabu, Y Murayama, and S. Matsumoto, "SF6 Insulation and its Application to HV Equipment", IEEE Transactions on Electrical Insulation, Vol. 26, No.3, pp 358-366, 1991.
- [8] Umar Khayam, Satoshi Matsumoto, Shinya Ohtsuka, Masayuki Hikita,"Partial Discharge Measurement in Three-phase Construction", IEEE International Conference on Properties and Application of Dielectric Material ICPADM 2006, Bali, Indonesia, 2006.
- [9] Umar Khayam,"Locus and Pattern of Electric Field Vector in the Insulation of Threephase Gas Insulated Switchgear", *IEEE International Conference on Power Engineering* and Renewable Energy, Bali, Indonesia, July 2012.
- [10] Umar Khayam, "Rotating Characteristicsof Electric Field Vector in Three-phase Power Apparatus", IEEE Conference on Condition, Monitoring, and Diagnosis, Bali, Indonesia, September 2012.
- [11] P.C.J.M. van der Wielen: "On-line Detection and Location of Partial Discharges in Medium-Voltage Power Cables", Doctoral Dissertation, T.U. Eindhoven, 2005.
- [12] Takayoshi Misaki, Hideki Yamamoto, Koshi Itaka,"An Analysis of Three Dimensional Asymmetric Field Distribution in SF6 Gas Insulated Cable", *IEEE Transaction on Power Apparatus and Systems*, Vol. PAS-92, pp. 2024-2031, 1973.
- [13] M.M.A. Salama, R. Hackam, A. Nosseir, A. Soliman, T. El-Shiekh,"Methods of Calculations of Field Stresses in a Three-core Power Cable", *IEEE Transaction on Power Apparatus and Systems*, Vol. PAS-103, No. 12, pp. 3434-3441, 1984.
- [14] M.M.A. Salama, R. Hackam, A. Nosseir,"Voltage Rating of a Three-core Power Cable from Consideration of Discharges in Voids", *IEEE Transaction on Power Apparatus and Systems*, Vol. PAS-103, No. 12, pp. 3442-3447, 1984.
- [15] N.H. Malik, A.A. al-Arainy, "Electrical Stress Distribution in Three-core Belted Power Cables", IEEE Transactions on Power Delivery, Vol. PWRD-2, No. 3, pp. 589-595, July 1987.
- [16] Okubo, S. Yanabu,"Development of Three Dimensional Electric Field Analysis by Segment Arrangement Based on Charge Simulation Method", *Journal IEEJ Vol. 110*, pp. 699-706, No. 10, 1990.

[17] Jesus A. Gomollon, Roberto Palau," Steady State 3-D-Field Calculations in Three-phase Systems With Surface Charge Method," *IEEE Transactions on Power Delivery, Vol. PWRD-20, No. 2, pp. 919-924, April 2005.*



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